

# 低渗透气藏克氏渗透率影响因素室内实验研究

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**摘要:** 含有二氧化碳的低渗透气藏的岩石物性及流体物性具有特殊性, 无法准确分析气体滑动效应对克氏渗透率和渗流能力的影响。为此, 采用室内单相气体渗流实验进行测定与分析。结果表明, 气体在岩心渗流过程中存在克氏效应, 岩心类型、围压、气体类别和温度是影响其克氏渗透率的主要因素。孔隙型岩心的克氏渗透率远大于微裂缝—孔隙型岩心的克氏渗透率。随着实验围压的增大, 气测渗透率与气体平均压力倒数关系曲线的斜率不变, 但是克氏渗透率及其变化幅度逐渐减小。由于气体的相对分子质量不同, 二氧化碳的克氏渗透率大于天然气和氮气的克氏渗透率。在相同的实验围压和实验岩心条件下, 实验温度越高, 其对气体渗流的影响越小, 即 20℃ 时岩心的克氏渗透率大于 50、80 和 140℃ 下岩心的克氏渗透率。

**关键词:** 低渗透气藏 克氏渗透率 气体滑动效应 影响因素 克氏效应

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通常把平均渗透率低于  $10 \times 10^{-3} \mu\text{m}^2$  的气藏称为低渗透气藏, 其分布广泛, 种类繁多<sup>[1-2]</sup>。在吉林油田深层火山岩储层发现了含有二氧化碳的长岭、红岗、孤店等天然气田, 目前已知其天然气控制储量达到  $600 \times 10^8 \text{ m}^3$ <sup>[3-4]</sup>。该类低渗透气藏的发现, 增大了吉林油田的天然气储量, 提高了油田的发展潜力。

克林肯贝格提出了气体在微管中流动时存在滑动效应, 认为在管壁处的气体分子有的仍处于运动状态, 并不是全部粘附于管壁上<sup>[4-8]</sup>。气体平均压力越小, 气体分子间的相互碰撞越少, 气体的滑动效应就越严重; 如果气体平均压力增至无穷大, 气体的流动性质越接近于液体的流动性质, 这时管壁上的气膜则趋于稳定, 气体滑动效应逐渐消失<sup>[4-8]</sup>。

气体渗流存在滑动效应, 主要表现在: 不同气体、不同压力 and 不同物性岩心条件下所测的渗透率不同<sup>[9-11]</sup>。由于岩石物性及流体物性的特殊性, 该类低渗透气藏的开发难度较大, 并且中国对这类气藏的开发经验不足<sup>[12-13]</sup>。因此, 笔者对火山岩气藏的气体滑动效应和克氏渗透率的影响因素进行了研究, 以期该类低渗透气藏的合理、高效开发提供依据。

## 1 实验器材与方案

### 1.1 实验器材

主体实验装置为 CFS-200 多功能综合驱替系统, 附属设备包括气量计、真空泵等。

实验岩心采用长深气藏和徐深气藏的全直径岩心, 岩心物性参数如表 1 所示, 并按照 SY/T 5336—2006<sup>[14]</sup> 分别测定其孔隙度和渗透率。

表 1 实验岩心物性参数

| 岩心<br>编号 | 岩心类型   | 直径/<br>cm | 长度/<br>cm | 孔隙<br>度/% | 气测渗透率/<br>$10^{-3} \mu\text{m}^2$ |       |
|----------|--------|-----------|-----------|-----------|-----------------------------------|-------|
|          |        |           |           |           | 水平方向                              | 垂直方向  |
| I-1      | 孔隙     | 10.282    | 19.40     | 8.5       | 0.108                             | 0.021 |
| I-2      | 孔隙     | 10.164    | 21.15     | 5.4       | 0.017                             | 0.013 |
| I-3      | 孔隙     | 10.158    | 18.89     | 7.5       | 0.024                             | 0.009 |
| II-1     | 微裂缝—孔隙 | 10.224    | 18.20     | 3.0       | 0.042                             | 0.006 |
| II-2     | 微裂缝—孔隙 | 10.172    | 22.35     | 3.6       | 0.030                             | 0.012 |
| II-3     | 微裂缝—孔隙 | 10.126    | 19.77     | 3.6       | 0.010                             | 0.092 |

### 1.2 实验方案

实验方案包括: ①不同类型(孔隙型、微裂缝—

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孔隙型) 岩心的气体渗流实验, 实验温度为  $20\text{ }^{\circ}\text{C}$ , 实验气体为天然气; ②不同围压条件下的气体渗流实验, 实验温度为  $80\text{ }^{\circ}\text{C}$ , 实验气体为天然气; ③不同气体(二氧化碳、天然气、氮气) 的渗流实验, 实验温度为  $80\text{ }^{\circ}\text{C}$ , 实验围压为  $2\text{ MPa}$ ; ④不同温度下的气体渗流实验, 实验气体为天然气, 实验围压为  $2\text{ MPa}$ 。

## 2 影响因素

### 2.1 岩心类型

由不同岩心的气测渗透率与天然气平均压力倒数的关系(图1)可以看出: ①在岩心和气体均相同的条件下, 采用不同气体压力所测定的气测渗透率不同, 并且岩心的气测渗透率与气体平均压力倒数成线性正相关; ②不同类型的岩心气测渗透率差别很大, 在相同的气体压力下, 孔隙型岩心的气测渗透率远大于微裂缝—孔隙型岩心的气测渗透率, 并且孔隙型岩心的克氏渗透率( $0.35 \times 10^{-3} \sim 0.48 \times 10^{-3}$

$\mu\text{m}^2$ ) 远大于微裂缝—孔隙型岩心的克氏渗透率( $0.001 \times 10^{-3} \sim 0.008 \times 10^{-3} \mu\text{m}^2$ )。这些现象表明, 在气测岩心渗透率过程中, 岩心内部发生气体滑动, 则气体在岩心中流动时存在克氏效应。由于孔隙型岩心为基质孔隙度较大的岩心, 岩心孔隙的连通性较好, 且存在良好的渗流通道, 其气测渗透率明显偏大。而微裂缝—孔隙型岩心为基质致密含有微裂缝的双重介质岩心, 当气体压力增大到一定程度时, 其气测渗透率仍然很低。这是因为微裂缝—孔隙型岩心虽然含有微裂缝, 但是微裂缝的连通性不是很好, 所以在气体渗流过程中微裂缝无法起到增强气体流动的作用。

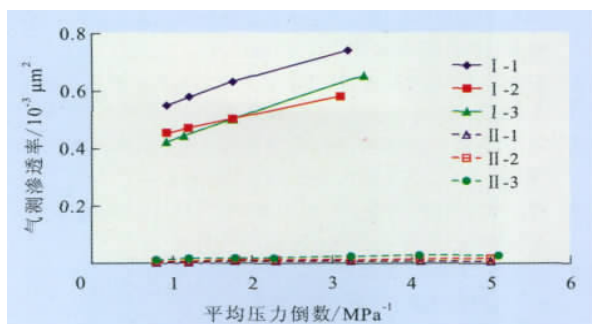


图1 不同类型岩心的气测渗透率与气体平均压力倒数的关系

### 2.2 围压

随着气体平均压力的增加, 不同实验围压条件

下的岩心气测渗透率变化趋势相同, 气测渗透率与气体平均压力倒数成线性正相关(图2)。随着实验围压的增加, 气测渗透率与气体平均压力倒数关系曲线的斜率不变; 实验围压越大, 该条件下岩心的克氏渗透率越小( $0.005 \times 10^{-3} \sim 0.001 \times 10^{-3} \mu\text{m}^2$ ), 并且克氏渗透率的减小幅度呈递减趋势。这是因为低渗透岩心具有孔径小、比表面积大等特点, 随着实验围压的增大, 岩心受到压缩使其直径、孔隙度等物性参数发生变化, 导致气体在岩心中流动困难, 气测渗透率变小; 随着实验围压的继续增大, 岩心的压缩系数和孔隙度的减小幅度变大, 测得的气测渗透率的减小幅度增大, 则克氏渗透率越小。

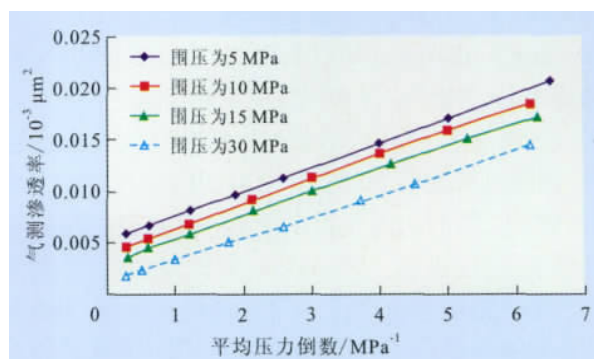


图2 不同围压下的气测渗透率与气体平均压力倒数的关系

### 2.3 驱替气体

从不同驱替气体条件下的气测渗透率与气体平均压力倒数的关系(图3)可以看出, 二氧化碳的气测渗透率与气体平均压力倒数的关系曲线明显不同于天然气、氮气的气测渗透率与气体平均压力倒数的关系曲线, 前者曲线的斜率小于后两者, 而后两者的气测渗透率与气体平均压力倒数曲线斜率基本相同。由图3可求得二氧化碳、天然气和氮气的克氏渗透率分别为 $0.255 \times 10^{-3}$ 、 $0.235 \times 10^{-3}$ 和 $0.205 \times 10^{-3} \mu\text{m}^2$ 。分析后认为: 当气体的平均压力相同时,

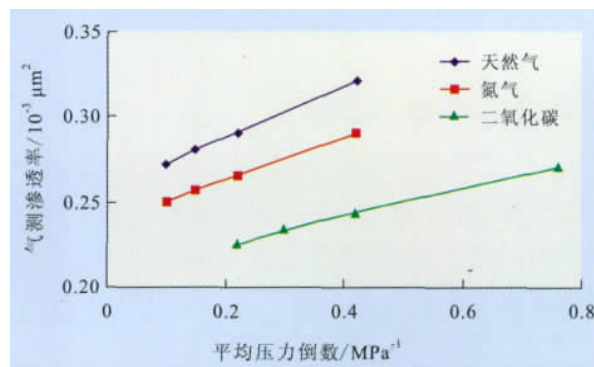


图3 不同驱替气体下的气测渗透率与气体平均压力倒数的关系

岩心孔隙中气体分子的相对分子质量越小,气体分子间相互碰撞的次数就越少,使得气体更加容易流动,气体的滑脱现象就越严重,气体的流量也就越大,则气测渗透率越大;由于二氧化碳的相对分子质量大于天然气和氮气的相对分子质量,所以二氧化碳的克氏渗透率小于天然气和氮气的克氏渗透率。

## 2.4 温度

在其他实验条件不变的情况下,实验温度对气测渗透率与气体平均压力倒数的关系曲线影响显著(图4),岩心的克氏渗透率明显不同。在20℃条件下,岩心的克氏渗透率为 $0.48 \times 10^{-3} \mu\text{m}^2$ ,明显大于50℃下岩心的克氏渗透率( $0.3 \times 10^{-3} \mu\text{m}^2$ );而80

和140℃时岩心的克氏渗透率较为接近,约为 $0.24 \times 10^{-3} \mu\text{m}^2$ 。由图4还可以看出,实验温度越低,气测渗透率与气体平均压力倒数关系曲线越陡,20℃时的曲线斜率大于140℃时的曲线斜率;实验温度越高,曲线斜率越小,50与80℃时的曲线斜率较为接近,而140℃时的曲线斜率最小。这是因为在低压条件下,温度越高,气体的粘度越大,越不利于气体在岩心孔隙中流动,所以气体的流量越小,所测得的克氏渗透率就越小。在相同的实验围压和实验岩心条件下,实验温度越高,其对气体渗流的影响越小;并且随着实验温度的升高,气测渗透率与气体平均压力倒数关系曲线间的变化幅度明显减小。

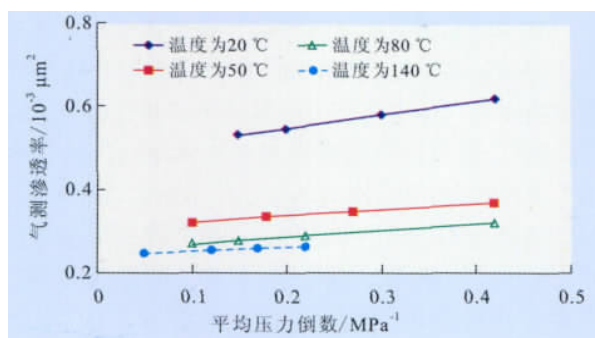


图4 不同温度下的气测渗透率与气体平均压力倒数的关系

## 3 结论

气体在岩心渗流过程中存在克氏效应,气测渗透率与气体平均压力倒数成线性正相关,其克氏渗透率取决于孔隙度、渗透率等岩心自身的物理特性。

其中孔隙型岩心的克氏渗透率远大于微裂缝—孔隙型岩心的克氏渗透率。

随着实验围压的增加,气测渗透率与气体平均压力倒数曲线的斜率相同,但是其克氏渗透率逐渐减小,并且减大幅度呈递减趋势,这是由低渗透岩心的物性所决定的。

气体相对分子质量对渗透率与平均压力倒数曲线有明显影响,二氧化碳的克氏渗透率大于天然气和氮气的克氏渗透率。

温度也是影响岩心气体克氏渗透率的重要因素,20℃时岩心的克氏渗透率大于50、80和140℃时岩心的克氏渗透率。

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19(2):81–83.

**Abstract:** Inadequate natural energy and poor transmission of pressure will give rise to deep pressure decline after putting into development in low permeable reservoir. Pressure decline will induce damages to rock physical properties and flowing character, i. e. reservoir rock presents stress sensitivity. Simulating changing process of reservoir pressure by flowing test, threshold pressure gradients at different effective overburden pressures are tested, and relationship between threshold pressure gradients and effective overburden pressures is studied. With mercury-injection test, nuclear magnetic resonance spectrometry analysis and rock mechanics test, changing mechanism for threshold pressure gradients in changing process of reservoir pressure is thoroughly analyzed. It was understood that, the threshold pressure gradients increases with reservoir pressure declines, i. e. threshold pressure gradients is sensitive to stress. It is also indicated that the lower the rock permeability, the bigger the increasing amplitude of threshold pressure gradients, which means that the stress sensitivity is stronger. It is suggested that, when calculating rational spacing between wells, it is necessary to consider the effect of reservoir pressure maintenance level on threshold pressure gradients.

**Key words:** low permeability; threshold pressure gradient; stress sensitivity; net overlying pressure; pore throat

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**Zhang Xing, Yang Shenglai, Zhang Ling et al. Experimental study on factors of KlinKenberg permeability in low permeable gas reservoir. *PGRE*, 2012, 19(2):84–86.**

**Abstract:** CNPC found a low-permeability gas reservoir with CO<sub>2</sub> in Jilin oil fields. Because the rock properties and fluid properties are unique, it is not accurate to analysis the effects of gas slippage effect on KlinKenberg permeability and penetration capacity. In view of this specificity, they are determined and analyzed by single-phase gas flow laboratory experiments. Experimental studies show that the KlinKenberg effect is found in the gas flow process in core and the influence factors are important including the core type, confining pressure, gas type and temperature. The KlinKenberg permeability of porosity core is higher than that of micro-fracture core. With the increasing of confining pressure, the slop of permeability-mean pressure curve is not changed, but the KlinKenberg permeability and its amplitude are decreased. Because of the different molecular weights, the KlinKenberg permeability of carbon dioxide (big molecular weight) is higher than that of natural gas and nitrogen gas (small molecular weight). The influence of temperature on gas flow at low temperature is greater than that at high temperature, that is, the KlinKenberg permeability of 20 °C is higher than that of 50, 80 and 140 °C.

**Key words:** low-permeability gas reservoir; KlinKenberg permeability; gas slippage effect; influence factor; KlinKenberg effect

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**Li Lianjiang. Study on drainage gas pattern for offshore gas wells, Chengdao oilfield. *PGRE*, 2012, 19(2):87–89.**

**Abstract:** After the condensate gas wells have been flooded, the choice of drainage gas recovery plan must be considered with the specific production environmental restrictions. In the paper, according to different stages conditions of the liquid production and gas production in a condensate gas well, the approximate drainage gas process pattern for offshore gas wells is studied by the well-bore temperature and pressure drop models. And, an effective feasible and economic drainage gas technology, the electric pump drainage gas recovery scheme, is put forward. Through the implementation of drainage gas recovery scheme, the natural gas output of the well is improved. The drainage gas schemes adopted by the gas well at different production stage can also be referenced for other gas wells nearby.

**Key words:** condensate gas wells; pressure drop model; temperature drop model; water-out gas production technique; Chengdao oilfield

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**Zhuang Li, Zhang Ling. Growth trend study of proved oil and gas reserves based on the upgrade rate of probable reserves. *PGRE*, 2012, 19(2):90–92.**

**Abstract:** Oil and gas reserves growth trend prediction research is the key factor for the oil company to make exploration and development strategy. From the study of contribution of probable reserves to the increased proved reserves of one oil company for ten years, it shows a steady rate at about 50% in the last three years. Upgrade rate of probable reserves can be classified into yearly increased and accumulative probable reserves upgrade rate. Research shows that the accumulative probable reserves upgrade rate has more significant meaning for the prediction of the growth of incased proven reserves next year. Considering the quality of increased probable reserves is very close in the recent years, based on the relationship of increased proved reserves with the accumulative probable reserves, a formula is summarized for the prediction of increased proved reserves, with convincing results tested with actual data. This method can be used by the exploration and development decision-making departments.

**Key words:** controlled reserve; proved reserve; contribution of controlled reserve; upgrading of controlled reserve; reserve prediction

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**Wang Shuhua, Wei Ping. SEC reserves dynamic evaluation and analysis. *PGRE*, 2012, 119(2):93–94.**

**Abstract:** Since Sinopec's public offering in New York and London in 1999, there are great challenges to bring domestic reserves management more in line with international practice, SEC methods and concepts of oil and gas reserves evaluation are having great shock on the domestic reserves calculation and management. Based on our decade years' experiences in domestic reserves calculation, examination and SEC reserves evaluation, this paper analyzes 5 methods in SEC reserves evaluation: analogy, volume, production decline, material balance and reservoir modeling methods; herein, we present the object, basis, scope and conditions in