文章编号:1009-9603(2021)01-0132-05

DOI:10.13673/j.cnki.cn37-1359/te.2021.01.016

预测页岩气井产量和可采储量泛指数 递减模型的建立及应用

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摘要:随着中国页岩气工业的发展和大量页岩气井的投产,如何有效地预测页岩气井的产量和可采储量已成为油 气藏工程的重要课题,也是页岩气资源的生产和管理部门极为关心的问题。由于页岩气是以吸附状态和自由状态 分别储存于超致密页岩基质和次生裂缝系统中,而页岩气井在钻井、完井、测井和压裂过程中受到泥浆的多次污 染。因此,投产后的页岩气井表现出明显的独立性、差异性和复杂性。再者,由于页岩气井以降压解吸和能量消耗 式开采,具有投产即进入递减的特征,因此,产量递减法已成为首选的评价方法。基于陈元千等提出的广义单峰周 期预测模型,经简化后得到预测页岩气井产量和可采储量的泛指数递减模型。该模型的递减指数m为0~1。当 m=1时为著名的指数递减模型;当m=0.5时可得具有实用价值的0.5型泛指数递减模型。对于具体的非常规气井, 在实际预测中,需要利用生产数据通过线性迭代试差法,确定a和c及m值。根据美国宾州 Marcellus页岩气藏两口 页岩气井生产数据,利用泛指数递减模型,对页岩气井的产量和可采储量进行预测。结果表明,建立的泛指数递减 模型是实用有效的。

关键词:页岩气;产量;可采储量;泛指数递减模型;应用 中图分类号:TE32*8 **文献标识码:**A

Establishment and application of pan exponential decline model for forecasting production rate and recoverable reserves of shale gas wells

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Abstract: With the advancement in China's shale gas industry and the large-scale production of shale gas wells, how to effectively forecast the production rate and recoverable reserves of shale gas wells and has become a crucial subject of oil and gas reservoir engineering. It is also a matter of great concern to shale gas production and management departments. As shale gas is stored in the ultra-tight shale matrix and the secondary fracture system in the adsorption state and the free gas state, respectively, it can be polluted by mud during the drilling, completion, logging, and fracturing. Therefore, the shale gas wells that have been put into production show obvious independence, diversity, and complexity. More importantly, shale gas wells are brought into production by desorption after pressure drops and energy consumption featured by the decreasing production at the moment it starts. Consequently, the production decline method has become the first choice for evaluation. In this paper, the generalized single peak cycle model proposed by Chen Yuanqian et al.is simplified into a pan exponential decline model (PEDM) that can forecast the production rate and recoverable reserves of shale gas wells. The decline exponent *m* ranges from 0 to 1. At *m*=1, it is the famous exponential decline model. At *m*=0.5, it is the 0.5-PEDM of practical

收稿日期:2020-05-15。

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value. For specific unconventional shale gas wells, it is necessary to use production data to determine the values of a, c, and m by linear iterative trial and error method in actual forecasting. The application of production data from two wells in the Marcellus shale gas reservoir, Pennsylvania, the US, elicits the effectiveness of the PEDM in forecasting the production rate and recoverable reserves of shale gas wells.

Key words: shale gas; production rate; recoverable reserves; pan exponential decline model; application

非常规页岩气藏由超致密的基质和次生裂缝 组成。页岩气分别以吸附状态和自由状态储存于 这两种介质中。页岩气的产量及其递减的快慢除 与基质的吸附气含量和次生裂缝发育程度有关外, 还与水平井的钻井、完井和压裂效果有关。页岩气 井的开采表现为定容、封闭、消耗式和投产即进入 递减的特点。因此,利用线性递减模型^[1-2]、广义递 减模型^[3]和幂函数递减模型^[4]预测页岩气井产量和 可采储量均取得了较好效果。为此,基于广义单峰 周期预测模型^[5],建立预测页岩气井产量和可采储 量的泛指数递减模型,并介绍该模型的派生、无因 次产量曲线和模型的求解方法。

1 泛指数递减模型的建立

在广义翁氏模型^[6]、威布尔模型^[7]、陈-郝模型^[5] 和瑞利模型^[8]的基础上,陈元千等建立了广义单峰 周期预测模型^[5],其中产量、峰值产量、峰值出现时 间和可采储量计算式分别为:

$$q = at^{b} \mathrm{e}^{-t^{m}/c} \tag{1}$$

$$q_{peak} = a \left(\frac{bc}{2.718m}\right)^{1/m} \tag{2}$$

$$t_{peak} = \left(\frac{bc}{m}\right)^{1/m} \tag{3}$$

$$G_{R} = \frac{ac^{(b+1)/m}}{m}\Gamma\left(\frac{b+1}{m}\right)$$
(4)

由(1)式—(4)式可以看出,广义单峰周期预测 模型有a,b,c和m四个常数。其中常数a控制峰值 的高低,a值愈大峰值产量愈高,反之愈低。常数b 控制峰位,b值愈大,峰位距纵轴愈远,反之愈近。 常数c控制峰值后产量递减的快慢,c值愈大产量递 减愈慢,反之愈快。时间指数m用于判别模型的类 别:当m=1时可得广义翁氏模型;当m=2时可得陈-郝模型;当m=b+1时可得威布尔模型;当m=2且b=1 时可得瑞利模型。对于广义单峰周期预测模型,当 b=0时即得投产进入递减的泛指数递减模型。 泛指数递减模型的产量和可采储量计算公式 分别为:

$$q = a \mathrm{e}^{-t^m/c} \tag{5}$$

$$G_R = \frac{ac^{1/m}}{m} \Gamma\left(\frac{1}{m}\right) \tag{6}$$

由(6)式可见, G_R 与a和 $c^{1/m}$ 均成正比, 与m成反比。

在(6)式中的Γ(1/m)值可查伽马函数表或由 相关经验公式^[9]求得,相关经验公式为:

$$\Gamma\left(\frac{1}{m}\right) = \Gamma(Z+1) = \frac{2.507(Z+2)^{Z+0.5}}{e^{Z+2}} \times \left(\frac{1.0864}{Z+1} + 1\right)$$
(7)

其中:

$$Z = \frac{1 - m}{m} \tag{8}$$

由(5)式对时间求导得:

$$\frac{\mathrm{d}q}{\mathrm{d}t} = -\frac{mq}{ct^{1-m}} \tag{9}$$

Arps 定义的递减率^[10]为:

$$D = -\frac{\mathrm{d}q}{q\mathrm{d}t} \tag{10}$$

将(9)式代入(10)式得泛指数递减模型的递减 率为:

$$D = \frac{m}{ct^{1-m}} \tag{11}$$

由(11)式可以看出,泛指数递减模型的递减率 与m成正比,与c成反比。当t=0时,初始递减率趋 近于无穷大。

2 泛指数递减模型的派生

当 *m*=0.5 时, Γ(1/*m*)=1.0, 由(5)式、(6)式和 (11)式可得具有实用价值的0.5 型泛指数递减模 型,其产量、可采储量和递减率计算式分别为:

$$q = a \mathrm{e}^{-\iota^{0.5}/c} \tag{12}$$

$$G_R = 2ac^2 \tag{13}$$

$$D = \frac{0.5}{ct^{0.5}}$$
(14)

当*m*=1时,Γ(1/*m*)=1.0,由(5)式、(6)式和(11) 式可得著名的指数递减模型,其产量、可采储量和 递减率计算式分别为:

$$q = a \mathrm{e}^{-t/c} \tag{15}$$

$$G_{R} = ac \tag{16}$$

$$D = \frac{1}{c} \tag{17}$$

3 泛指数递减模型的无因次关系

为了建立泛指数递减模型的无因次产量曲线, 首先将(5)式改写为:

$$q = a e^{-c^{m-1}(t/c)^m}$$
(18)

泛指数递减模型的无因次产量和无因次时间 分别为:

$$q_D = \frac{q}{q_0} \tag{19}$$

$$t_D = \frac{t}{2} \tag{20}$$

将(19)式和(20)式代入(18)式,且由(15)式可 以看出,当t=0时, $q = a = q_0$,由此得泛指数递减模 型的无因次产量与无因次时间之间的关系式为:

$$q_{D} = e^{-c^{m-1}t_{D}^{m}}$$
(21)

由(21)式可以看出:当m=0时, q_D 为常数;当m=1时, $q_p = e^{t_p}$, q_p 为指数递减。当取c=5时,由(21)式 求得不同m值时 q_p 与 t_p 的无因次关系(图1);当m=0.5时,由(21)式求得不同c值时 q_p 与 t_p 的无因次关 系(图2)。由图1和图2可以看出,m值比c值对 q_p 的影响明显。



4 泛指数递减模型的求解方法

由(5)式可以看出,泛指数递减模型是带有 a和



c及m三个常数的非线性递减模型,需根据实际生产数据,利用线性迭代试差法进行求解。为此,首先将(5)式等号两端同时取自然对数得:

$$\ln q = \ln a - \frac{1}{c} t^m \tag{22}$$

若设:

$$\alpha = \ln a \tag{23}$$

$$c = \frac{1}{\beta} \tag{24}$$

则得:

$$\ln q = \alpha - \beta t^m \tag{25}$$

再利用(25)式进行线性迭代试差法求解。当*m* 值为0~1时,可按步长为0.05 给定不同的*m*值,求 得相关系数最高直线的*m*值,即为欲求的正确*m*值, 并由(25)式进行线性回归,确定直线的截距α、斜率 β和相关系数*R*²。最后,由(23)式和(24)式分别确 定*a*和*c*值。

5 应用实例

将美国宾州 Marcellus 页岩气藏的 M₁和 M₂井投 产后的产量递减数据^[11]绘于图 3,利用线性迭代试 差法,由(25)式求得两口井的最佳直线关系并绘于 图 4。由图 4 的线性回归求得:M₁井的 m 值为 0.5,α





Fig.4 The optimal linear $\ln q - t^m$ relations of M_1 and M_2 wells

值为6.4606,β值为0.2805,相关系数为0.9900;M₂ 井的m值为0.5,α值为5.8373,β值为0.2779,相关 系数为0.9940。由(23)式和(24)式分别求得两口 井的a和c值:M₁井的a和c值分别为639.44和3.57; M₂井的a和c值分别为342.85和3.60。将两口井的 a,c和m值分别代入(5)式,得M₁和M₂井的产量预 测公式分别为:

$$q = 639.44 \times e^{-t^{0.5/3.57}}$$
(26)

$$q = 342.85 \times e^{-\iota^{0.5}/3.60}$$
(27)

由(26)式和(27)式分别预测两口井的理论产 量并绘于图3。由图3可以看出,预测曲线与实际数 据符合得很好。

将 M₁和 M₂井的 *m*和 *c* 值分别代入(11)式,将预 测得到的两口井的递减率绘于图 5。由图 5 可见,两 口井的递减率随时间的变化基本一致,这与两口井 的*m*和 *c* 值均基本相同有关。



将 M_1 和 M_2 井的m值代入(7)式,可得两口井的 完全伽马函数, $\Gamma(1/m)=\Gamma(2)=1.0$ 。将2口井的完全 伽马函数值以及a,c和m值分别代入(6)式,可得 M_1 和 M_2 井的可采储量分别为:

$$G_R = \frac{639.44 \times 3.57^{1/0.5}}{0.5} \times 1.0 =$$

16 299 × 10⁴ = 1.629 9 × 10⁸ m³ (28)

$$G_R = \frac{342.85 \times 3.60^{1/0.5}}{0.5} \times 1.0 =$$

8 887 × 10⁴ = 0.888 7 × 10⁸ m³ (29)

6 结论

通过对广义单峰周期预测模型的简化,得到预测页岩气井投产即进入递减的泛指数递减模型。 该模型适用性较强,可对不同页岩气井的产量、可 采储量和递减率进行预测。泛指数递减模型的递减指数为0~1。随着m值的增加,产量的递减率增加,随着c值的增加,产量的递减率减小。由m=0.5 和m=1可分别得到0.5型的泛指数递减模型和著名的指数递减模型。由于M₁和M₂井的m和c值均基本相同,因而两口井的递减率几乎是重合的。实例应用结果表明,所建立的泛指数递减模型是实用有效的。

符号解释

a——广义单峰周期预测模型和泛指数递减模型的产量 常数,10⁴ m³/mon;

b——广义单峰周期预测模型的峰位指数,dim;

c——广义单峰周期预测模型和泛指数递减模型的时间 常数, mon;

D----递减率,mon⁻¹;

 G_R ——页岩气井可采储量, 10⁴ m³;

m——泛指数递减模型的时间指数,dim;

- q---页岩气井产量,104 m3/mon;
- q0----当t=0时的初始理论产量,104 m3/mon;
- q_D ——无因次产量,dim;
- q_{peak}——广义单峰周期预测模型的峰值产量,10⁴ m³/mon;
- R²——相关系数,dim;
- t——生产时间,mon;
- t_D ——无因次时间,dim;

 t_{peak} 一广义单峰周期预测模型峰值出现的时间,mon; Z——完全伽马函数的变量;

 α 和 β ——泛指数递减模型最佳直线的截距和斜率;

 $\Gamma(Z+1)$ ——完全伽马函数。

参考文献

[1] 陈元千,周翠.线性递减类型的建立、对比与应用[J].石油学报,2015,36(8):983-987.

CHEN Yuanqian, ZHOU Cui. Establishment, comparison and application of the linear decline type[J].Acta Petrolei Sinica, 2015, 36(8):983–987.

[2] 陈元千,齐亚东,傅礼兵,等.井控页岩气可动地质储量和可采 储量的评价方法[J].油气地质与采收率,2018,25(4):73-78.

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CHEN Yuanqian, QI Yadong, FU Libing, et al. Methods for estimating well-controlled movable in -place and recoverable reserves of shale gas[J].Petroleum Geology and Recovery Efficiency, 2018, 25(4):73-78.

 [3] 陈元千,唐玮.广义递减模型的建立及应用[J].石油学报, 2016,37(11):1410-1413.
 CHEN Yuanqian, TANG Wei. Establishment and application of

generalized decline model [J]. Acta Petrolei Sinica, 2016, 37 (11):1410-1413.

[4] 陈元千,傅礼兵.幂函数递减模型的建立、对比与应用[J].油气 地质与采收率,2019,26(6):87-91.

CHEN Yuanqian, FU Libing. Establishment, comparison and application of power function decline model [J]. Petroleum Geology and Recovery Efficiency, 2019, 26(6):87–91.

[5] 陈元千,郝明强.多峰预测模型的建立与应用[J].新疆石油地质,2013,34(3):296-299.
 CHEN Yuanqian, HAO Mingqiang.Establishment and application

of the multi-peak forecasting model[J].Xinjiang Petroleum Geology,2013,34(3):296–299.

 [6] 陈元千.对翁氏预测模型的推导及应用[J].天然气工业,1996, 16(2):22-26,102.
 CHEN Yuanqian. Derivation and application of Weng's predica-

tion model[J].Natural Gas Industry, 1996, 16(2):22-26, 102. [7] 陈元千, 胡建国. 预测油气田产量和储量的 Weibull 模型(为纪 念克拉玛依油田勘探开发40周年而作)[J].新疆石油地质, 1995,16(3):250-255,287.

CHEN Yuanqian, HU Jianguo. Weibull model for predicting output and reserve in an oil and gas field [J].Xinjiang Petroleum Geology, 1995, 16(3): 250–255, 287.

[8] 陈元千.瑞利模型的完善推导与应用[J].油气地质与采收率, 2004,11(4):39-41.

CHEN Yuanqian. The perfect derivation of Rayleigh model and its application [J]. Petroleum Geology and Recovery Efficiency, 2004, 11(4): 39-41.

- [9] LANCZOS C A. Precision approximation of gamma function [J]. Journal of the Society for Industrial and Applied Mathematics: Series B, Numerical Analysis, 1964: 1 186–1 196.
- [10] ARPS J J.Analysis of decline curves, Trans[J].AIME, 1945, 160: 228-247.
- [11] 何培,冯连勇,TOM Wilber.马塞勒斯页岩气藏单井产量递减 规律及可采储量预测[J].新疆石油地质,2015,36(2):249-252.

HE Pei, FENG Lianyong, TOM Wilber. Production decline rule and recoverable reserves prediction of Marcellus shale gas well in a production unit, Pennsylvania, US[J].Xinjiang Petroleum Geology, 2015, 36(2):249–252.

编辑 常迎梅

(上接第63页)

FANG Gang, LIU Baigen. Research on aquifers characteristics and hydraulic connection based on multiple drilling pumping tests in Balasu well field[J].Journal of China Hydrology, 2019, 39 (3):36-40,67.

- [23] 张国伟.基于抽水试验的上海第Ⅱ承压含水层特性分析[J].勘 察科学技术,2019,37(1):47-52.
 ZHANG Guowei.Characteristics analysis of the II confined aquifer in Shanghai based on pumping test[J].Site Investigation Science and Technology,2019,37(1):47-52.
- [24] CARDIFF M, BARRASH W, KITANIDIS P K, et al. A potentialbased inversion of unconfined steady-state hydraulic tomography [J].Ground Water, 2009, 47(2):259–270.
- [25] CARDIFF M, BARRASH W.Analytical and semi-analytical tools for the design of oscillatory pumping tests [J]. Ground Water, 2015,53(6):896-907.
- [26] BAKHOS T, CARDIFF M, BARRASH W, et al. Data processing for oscillatory pumping tests [J].Journal of Hydrology, 2014, 511: 310-319.
- [27] TEUTSCH G.An extended double-porosity concept as a practical modelling approach for a karstified terrain [C]//GUNAY G, JOHN-SON A I, BACK W.Hydrogeological processes in Karst Terranes.

Wallingford: IAHS Press, 1993: 281-292.

- [28] LIEDL R, SAUTER M, HÜCKINGHAUS D, et al. Simulation of the development of karst aquifers using a coupled continuum pipe flow model[J].Water Resources Research, 2003, 39(3):10–57.
- [29] BLACK J H, KIPP K L.Determination of hydrogeological parameters using sinusoidal pressure tests: A theoretical appraisal [J]. Water Resources Research, 1981, 17(3):686–692.
- [30] CARDIFF M, BAKHOS T, KITANIDIS P K, et al. Aquifer heterogeneity characterization with oscillatory pumping: Sensitivity analysis and imaging potential [J]. Water Resources Research, 2013, 49(9):5 395-5 410.
- [31] RENNER J, MESSAR M. Periodic pumping tests [J]. Geophysical Journal International, 2006, 167(1):479-493.
- [32] DAGAN G, RABINOVICH A.Oscillatory pumping wells in phreatic, compressible, and homogeneous aquifers [J]. Water Resources Research, 2014, 50(8):7058-7066.
- [33] RABINOVICH A, BARRASH W, CARDIFF M, et al. Frequency dependent hydraulic properties estimated from oscillatory pumping tests in an unconfined aquifer[J].Journal of Hydrology, 2015, 531:2–16.

编辑 邹潋滟