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I型有机质生油增压数学模型建立与应用

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摘要:生油增压定量化研究是计算油气成藏动力并进一步确定油气分布的关键。目前已有的生油增压计算方法较复杂或计算 精度不足,影响其在勘探中快速应用。基于 I 型有机质生烃特征综合分析,建立了生油增压数学模型,并将该模型应用于鄂尔 多斯盆地西峰油田长7段烃源岩生油增压的计算,同时分析了不同参数对生油增压的影响。结果显示,西峰油田长7段烃源岩 生油增压为4.6~14.8 MPa,地层压力与前人计算结果相近,说明模型具有较高的可靠性。参数敏感性分析表明,岩石压缩系 数对生油增压影响程度最大,为99.056%;总有机碳含量影响程度为0.342%;生烃影响因子和干酪根生油转化效率对生油增压 的影响程度分别为0.261%和0.250%;孔隙度和地层压力对生油增压的影响程度较小,分别为0.09%和0.001%。模型同时揭 示,较高的地层压力不利于生油增压,地层压力越高,增压越小。

关键词: 烃源岩; I 型有机质; 压缩性; 生油增压; 敏感性分析 文章编号: 1009-9603 (2023) 05-0057-06

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Establishment and application of mathematical model of oil generated overpressure by type I organic matter

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Abstract: Quantitative study on oil generated overpressure is the key to calculating the dynamics of oil and gas reservoirs and determining the distribution of oil and gas. The existing calculation methods of oil generated overpressure are low in calculation accuracy and complex, which affect their rapid applications in exploration. In this study, according to the comprehensive analysis of hydrocarbon generation characteristics of type I organic matter, a new mathematical model of oil generated overpressure was established. The model was used to calculate the oil generated overpressure of Chang7 source rock in Xifeng Oilfield of Ordos Basin and analyze the influence of different parameters on the oil generated overpressure. The results show that the oil generated overpressure of Chang7 source rock in Xifeng Oilfield is 4.6-14.8 MPa, and the formation pressure is similar to the previous calculation results, which indicates that the model is highly reliable. The sensitivity analysis of rock parameters shows that the rock compressibility factor has the greatest influence on the oil generated overpressure, with a value of 99.056%, followed by the total organic carbon content, with a value of 0.342%. The influence of hydrocarbon generation factor and kerogen oil-generating conversion efficiency on the oil generated overpressure, which is 0.09% and 0.001%, respectively. The model also reveals that higher formation pressure is not conducive to oil generated overpressure, and higher formation pressure makes the oil generated overpressure smaller. **Key words**: source rock; type I organic matter; compressibility; oil generated overpressure; sensitivity analysis

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含油气盆地的发育和形成与地层超压具有密切 的关系[1]。欠压实作用[2-4]、黏土矿物脱水[5-6]、有机质 生烃作用[7-10]、流体热增压作用[11-12]、构造应力[13]等是 超压形成的重要因素。有机质生烃作用不仅能增加 地层压力,同时还控制油气排出过程[14]。因此,建立 生油增压数学模型对分析油气运移及分布有重要意 义。BREDEHOEFT等在考虑油气的生成和排出基 础上,利用三维生油动力学模型验证了生烃作用对 犹他盆地地层超压的影响[15]。徐思煌等在质量守 恒、体积守恒和压力守恒3个原则约束情况下建立 了生油增压的数学模型,模型显示干酪根生成气态 经时产生的增压更加显著[16]。对于封闭条件较好的 烃源岩,生烃作用引起的超压达到岩石破裂压力时 会导致烃源岩产生裂缝,发生幕式排烃^[17]。BERG 等在岩石渗透率极低、应力状态稳定、生烃速率不变 和低温生油、高温生气的假设条件下建立了数学模 型,进一步肯定了生烃作用对幕式排烃的意义[18]。 郭小文等利用生油增压数学模型计算了生油增压, 并通过实验验证了生油增压模型的计算结果[19]。已 有研究成果从不同方面说明了生烃作用对超压及排 烃的重要性,但是这些模型或者数据需求量高导致 应用难度大,或者计算过于简化导致精度偏低。为 此,通过分析I型干酪根的生烃特征,重新建立生油 增压数学模型并获得解析解,同时分析控制生油增 压的主控因素,以期为油气成藏动力^[20]和烃源岩微 裂缝研究提供参考[21-23]。

1 生油增压模型推导

生油增压模型需遵循以下假设条件:①烃源岩 孔隙连通性较好。②I型干酪根生成的气体全部溶 解在原油中^[19]。③烃源岩受到的构造应力不变。④ 生烃过程中地层温度和埋藏深度不变。⑤生烃前后 干酪根压缩系数不变。

烃源岩生烃前,孔隙空间被地层水充满(图1a),则有:

$$V_{\rm w1} = \phi \tag{1}$$

孔隙中液态烃的质量可以表示为[19]:

$$M_{\rm o} = AFM_{\rm k1} \tag{2}$$

干酪根生油后原油的密度可表示为:

$$\rho_{o2} = \rho_o \left[1 + C_o \left(\Delta p + p_1 \right) \right]$$
(3)

则干酪根生成的原油体积表达式为:

$$V_{o2} = M_{o} / \rho_{o2} = AFM_{k1} / \left\{ \rho_{o} \left[1 + C_{o} (\Delta p + p_{1}) \right] \right\}$$
(4)

$$TOC = \frac{V_{\rm k} \rho_{\rm k}}{\rho_{\rm b} \kappa} \tag{5}$$

因此,干酪根生油前单位体积烃源岩中的干酪根体积*V*₄和质量*M*₄分别为:

$$V_{\rm k1} = \frac{TOC\,\rho_{\rm b}\,\kappa}{\rho_{\rm k}}\tag{6}$$

$$M_{\rm kl} = TOC\rho_{\rm b}\,\kappa\tag{7}$$

L

$$V_{o2} = AF \, TOC \,\rho_{\rm b} \,\kappa / \left\{ \rho_{\rm o} \left[1 + C_{\rm o} \left(\Delta p + p_{\rm 1} \right) \right] \right\} \tag{8}$$

系统温度不发生变化时,液体物态方程为[25]:

$$V = V_{o} \left[1 - \beta_{f} (p - p_{o}) \right]$$
(9)

则生油后孔隙中水的体积为:

$$V_{w2} = V_{w1}(1 - C_w \Delta p)$$
 (10)

$$V_{w2} = \phi(1 - C_w \Delta p) \tag{11}$$

干酪根一部分转化为原油,剩余的干酪根由于 孔隙压力增大受到压缩(图1b),因此生油后干酪根 的体积为:

$$V_{k2} = (1 - AF)(1 - C\Delta p)V_{k1}$$
(12)

将干酪根看作孔隙的一部分,则生油前后孔隙 体积的关系为:

 $V_{k2} + V_{o2} + V_{w2} = (1 + C_p \Delta p)(V_{w1} + V_{k1}) \quad (13)$ 将(1),(6),(8),(11),(12)式代入(13)式,整理 得:

$$\Delta p = \frac{-b + \sqrt{b^2 - 4ac}}{2a} \tag{14}$$

其中:

$$a = \rho_{o}C_{o}(\phi C_{p} + \phi C_{w} + V_{k1}C_{p}) + V_{k1}\rho_{o}C_{k}C_{o}(1 - AF)$$
(15)

$$b = (\rho_{\circ} + \rho_{\circ}C_{\circ}p_{1})(\phi C_{p} + \phi C_{w} + V_{k1}C_{p}) + \rho_{\circ}C_{\circ}V_{k1} - \rho_{\circ}V_{k1}(1 - AF)(C_{\circ} - C_{k} - C_{\circ}C_{k}p_{1})(16)$$

$$c = (\rho_{\circ} + \rho_{\circ}C_{\circ}p_{1})V_{k1} - AFM_{k1} - \rho_{\circ}V_{k1}(1 - AF)(1 + C_{\circ}p_{1})$$
(17)



2 应用实例

鄂尔多斯盆地西峰油田长7段烃源岩发育范围 大,有机质含量高、类型好,是鄂尔多斯盆地中生界 重要的油源岩^[26-27]。西峰油田地处鄂尔多斯盆地西 南部,区内长7段烃源岩厚度为120~160 m,*TOC* 为4%~8%,镜质组反射率(*R*_o)为0.7%~0.95%^[28], 具有较强的生烃能力。以西峰油田长7段烃源岩为 例,计算其成藏期生油增压。此外,需重新厘定部分 参数。

2.1 孔隙度

计算孔隙度倒数压实模型为[29]:

$$\frac{1}{\phi_1} = \frac{1}{\phi_0} + KZ \tag{18}$$

MAGARA 提出了孔隙度随埋深变化的指数模型^[30]:

$$\phi_1 = \phi_0 \mathrm{e}^{-cz} \tag{19}$$

研究认为,双元模型可以将孔隙度恢复至成藏 期。基于文献[31],利用双元模型恢复了西峰油田 12口井长7段烃源岩成藏期孔隙度。计算结果显 示,西峰油田长7段烃源岩成藏期孔隙度为22.48%~ 29.13%,平均为26.19%(表1)。

2.2 岩石压缩系数

矿物分析显示,鄂尔多斯盆地南部长7段泥页 岩矿物组成差异较小,黏土矿物含量为42.16%,石 英含量为27.75%,斜长石含量为18.46%,菱铁矿和 其他矿物含量为11.63%^[32]。基于各类矿物含量及压 缩系数可计算不同岩石的骨架压缩系数^[33]。西峰油 田长7段泥页岩黏土矿物、石英、斜长石和菱铁矿的 C_{s} 分别取9.09×10⁻⁵^[34],1.20×10⁻⁵^[33],3.00×10⁻⁵和8.60×10⁻⁵ MPa^{-1[35]}。西峰油田长7段烃源岩成藏期的岩石 压缩系数表达式为:

$$C_{\rm p} = \frac{\phi}{1 - \phi} \sum_{i=1}^{n} x_i C_{\rm si} \tag{20}$$

利用(20)式计算西峰油田长7段烃源岩成藏期的 C_{n} 为2.03×10⁻⁵ MPa⁻¹。

将生油增压参数(表2)代入(14)式,结果显示, 西峰油田长7段烃源岩最大埋深期生油增压为4.6~ 14.8 MPa,地层压力为29.6~42.0 MPa,地层压力计 算结果与前人研究结果(28.0~42.0 MPa)^[22]有较好 的吻合度,说明文中建立的模型具有较高的可靠性。 2.3 参数敏感性

为了分析生油增压模型参数的敏感性,以生油 增压变化程度为指标研究参数的敏感性。其参数敏 感性分析基准方案为:A为0.3,F为28%,TOC为 6%, ϕ 为26.2%, C_p 为2.03×10⁵ MPa⁻¹, p_1 为25 MPa。 将参数变化范围设定为10%~60%(表3),计算由此 引起的生油增压。

由于各参数量度不一致,引起的 Δp 差别较大, 难以直接确定各参数的敏感性。因此,提出运用 k_i 分析不同参数对 Δp 的影响, k_i 为 Δp 变化值与某参数 变化值之比。计算结果显示: C_p , TOC, A, F, ϕ 和 p_1 的 k_i 分别为11 247, 37.91, 29.89, 28.88, 10.28 和 0.09。将各敏感参数的 k_i 代入(19)式即可得到每个 参数的影响程度:

$$\alpha = \frac{k_i}{\sum_{i=1}^{6} k_i}$$
(21)

计算结果显示, C_p 对 Δp 的影响程度最大,为

Table	Paleoporosity restoration results of Chang / source rock in Xifeng Oilfield of Ordos Basin								
井号	$H_{T=100}/\mathrm{km}^{[36]}$	$H_{T=0}/{ m km^{[36]}}$	$\phi_{T=0}/0/0^{[36]}$	$\Delta\phi_{T=100}/\%$	$\phi_{\scriptscriptstyle T=100}$ /%				
自 234	2.728	2.272	22.35	1.62	23.97				
固 10	2.232	1.563	27.13	2.00	29.13				
葫90	2.409	1.293	25.05	1.86	26.91				
里 69	2.666	2.331	22.05	1.68	23.73				
岭 78	2.479	1.852	23.16	1.82	24.98				
木16	2.619	2.189	22.54	1.71	24.25				
亍10	2.302	1.653	26.82	1.95	28.77				
剖 23	2.493	1.643	22.98	1.79	24.77				
西17	2.569	2.109	26.68	1.74	28.42				
镇12	2.509	2.089	26.02	1.79	27.81				
镇探1	2.477	2.057	27.30	1.80	29.10				
庄10	2.629	1.804	20.81	1.67	22.48				

表1 鄂尔多斯盆地西峰油田长7段烃源岩古孔隙度恢复结果

注: $H_{T=100}$ 为长7段最大埋深期的深度; $H_{T=0}$ 为长7段现今深度; $\phi_{T=0}$ 为长7段现今孔隙度; $\Delta\phi_{T=100}$ 为长7段最大埋深期至今孔隙度变化量; $\phi_{T=100}$ 为长7段最大埋深期孔隙度。

		表2 鄂尔多	斯盆地西峰油田	长7段烃源岩	生油增压参数		
Table2	Basic parameter	rs of oil generate	d overpressure f	or Chang7 sour	rce rock in Xifen	g Oilfield of Ordo	s Basin
F/ %	$\rho_{\rm k}/(\rm g{\scriptstyle \bullet}\rm cm^{{\scriptscriptstyle -}3})$	$\rho_{\rm o}/(\rm g{\scriptstyle \bullet}\rm cm^{-3})$	$\rho_{\rm b}/(\rm g{\scriptstyle \bullet} \rm cm^{-3})$	$C_{\rm w}$ / MPa ⁻¹	$C_{\rm k}/{ m MPa^{-1}}$	$C_{\rm p}/~{\rm MPa^{-1}}$	$C_{\rm o}/~{\rm MPa^{-1}}$
28	1.2	0.9	2.451	4.40×10 ⁻⁴	1.40×10 ⁻³	2.03×10-5	2.20×10-3
		表3	生油增压数学构	莫型参数敏感	生分析		
	Table3 Se	ensitivity analysi	s table of mather	natical model of	of oil generated of	overpressure	
参数变化范围/%	$A/(\mathrm{mg}^{\bullet}\mathrm{g}^{\text{-}1})$	F/%	TOC	2/%	$\phi/\%$	$C_{\rm p}/{ m MPa^{-1}}$	p_1 /MPa
0	0.30	28.0	6.0		26.2	2.03×10 ⁻⁵	25.0
10	0.33	30.8	6.6		28.8	2.23×10-5	27.5
20	0.36	33.6	7.2		31.4	2.44×10 ⁻⁵	30.0
30	0.39	36.4	7.3	8	34.0	2.64×10-5	32.5
40	0.42	39.2	8.4	4	36.7	2.84×10 ⁻⁵	35.0
50	0.45	42.0	9.0	0	39.3	3.05×10 ⁻⁵	37.5
60	0.48	44.8	9.	6	41.9	3.25×10-5	40.0

99.056%,远大于其他参数,进一步证明了本次研究 考虑 C_{\circ} 的必要性。TOC的影响程度为0.342%,如果 不考虑 C_p , TOC对 Δp 具有最大的影响, A和F对 Δp 的影响程度接近,分别为0.261%和0.250%, o和 p1 对 Δp 的影响程度较小,分别为0.09%和0.001%。此 Λ, p_1 越高, Δp 越小, 即较高的地层压力抑制生油增 压。

3 结论

在分析I型干酪根生烃特征基础上建立了生油 增压数学模型,并且利用此模型计算了鄂尔多斯盆 地西峰油田长7段烃源岩生油增压。结果表明,鄂 尔多斯盆地西峰油田长7段烃源岩生油增压为4.6~ 14.8 MPa。地层压力计算结果与前人研究结果有较 好的吻合度,表明文中建立的模型具有较高的可靠 性。参数敏感性分析表明, C_p 对 Δp 影响程度最大, $TOC次之, A 和 F 对 \Delta p$ 的影响程度较小, $\phi 和 p_1 对 \Delta p$ 的影响程度最低。生油增压模型揭示,较高的地层 压力抑制生油增压。

符号解释

a,b,c——一元二次方程的3个系数;	
A——生烃影响因子,mg/g;	
C——沉积物压实常数;	
C_k ——干酪根压缩系数, MPa ⁻¹ ;	
C_{o} ——原油的压缩系数, MPa ⁻¹ ;	
C _p ——岩石压缩系数,MPa ⁻¹ ;	
C_{s} ——岩石骨架压缩系数, MPa ⁻¹ ;	

 C_{si} ——每种矿物的压缩系数, MPa⁻¹;

- C_w ——地层水的压缩系数, MPa⁻¹;
- F——干酪根生油转化率,%;
- *i*——矿物种类,*i*=1,2,…,*n*;
- *K*——压缩因子,1/m;
- k_i ——生油增压变化率;
- M_{k1}——生油前干酪根的质量,g;
- M.——孔隙中液态烃的质量,g;
- p——液体体积为V时对应的压力,MPa;
- p。——标准状况下的地层压力, MPa;
- p1——生油前地层压力, MPa;
- Δp ——生油增压, MPa;
- TOC----总有机碳含量,%:
- V——液体体积, cm3;
- V_k ——单位体积烃源岩中的干酪根体积, cm³;
- Vk1——生油前单位体积烃源岩中的干酪根体积, cm3;
- Vk2——生油后单位体积烃源岩中的干酪根体积, cm3;
- V.——标准状况下孔隙中的原油体积, cm³;
- V.,一一干酪根生成后的原油体积, cm3;
- V_{w1}——生油前孔隙中水的体积, cm3;
- V_{w2}——生油后孔隙中水的体积, cm3;
- *x_i*——每种矿物的含量,%;
- α ——参数影响程度,%;
- β_{f} ——液体密度,g/cm³;
- κ——干酪根转化因子,一般取1.2;
- $\rho_{\rm b}$ ——标准状况下烃源岩密度,g/cm³;
- $\rho_{\rm k}$ ——干酪根密度,g/cm³;
- ρ_{o} ——标准状况下原油密度,g/cm³;
- ρ_{o2} ——生油后原油被压缩后密度,g/cm³;
- *φ*——岩石孔隙度,%;
- *φ*,——岩石初始孔隙度,%;
- ϕ_1 —— 埋深为 Z 处的岩石孔隙度,%。

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