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CO₂-C₂H₆吞吐提高致密油藏采收率实验研究

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摘要:注CO₂已经成为致密油藏提高采收率的重要手段之一,相较于纯CO₂,部分烃类气体对原油的降黏及混相能力更强。为此,通过高温高压PVT实验研究了CO₂及复合气体(CO₂-C₂H₆)-原油的饱和压力及黏度的变化特征,并利用高温高压岩心吞吐实验揭示了不同气体介质、吞吐压力及吞吐轮次下原油动用程度。研究结果表明:复合气体中C₂H₆增强了气液两相混相能力,提高了CO₂降黏及溶解能力,原油流动性显著增加。复合气体中随着C₂H₆摩尔分数的增加,原油饱和压力由14.24 MPa增至18.02 MPa,提高了26.54%;原油黏度由23.68 mPa·s降至8.76 mPa·s。不同吞吐压力下复合气体(CO₂-C₂H₆)的采收率提高效果均强于纯CO₂的,且吞吐压力在最小混相压力附近采收率提高程度高于其他吞吐压力。复合气体(CO₂-C₂H₆)对孔隙半径为0.0001~0.001和0.01~1 μm孔隙中的原油动用程度强于纯CO₂的。

关键词:致密油藏;饱和压力;黏度;岩心实验;核磁共振技术

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Experimental study on enhancing oil recovery of tight reservoirs through CO₂-C₂H₆ huff and puff

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Abstract: CO₂ injection has become one of the most important methods of enhanced oil recovery in tight reservoirs, but some hydrocarbon gases have more viscosity-reducing and miscibility on oil compared to pure CO₂. Therefore, this article studied the saturation pressure and viscosity changes of oil with CO₂ and composite gas (CO₂ and C₂H₆) by PVT experiments at high-temperature and high-pressure and revealed the percentage of producing oil with different gases, huff and puff pressures, and rounds by core huff and puff experiments at high-temperature and high-pressure. The results show that the C₂H₆ in the composite gas enhances the gas and liquid miscibility, improves the CO₂ viscosity reduction and dissolution ability, and significantly increases the fluidity of oil. With the increase of C₂H₆ mole fraction in the composite gas, the saturation pressure of oil increases by 26.54% from 14.24 MPa to 18.02 MPa, and the viscosity of crude oil decreases from 23.68 mPa·s to 8.76 mPa·s. Under different huff and puff pressures, the oil recoveries of composite gas (CO₂ and C₂H₆) are better than that of pure CO₂, and the increase of recovery near the minimum miscibility pressure is higher than under other huff and puff pressures. The percentage of producing oil by composite gases is higher

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than that of pure CO₂ in the pores of 0.0001-0.001 μm and 0.01-1 μm.

Key words: tight reservoir; saturation pressure; viscosity; core experiment; nuclear magnetic resonance (NMR)

随着全球经济发展的日益加速以及工业技术的不断发展,油气消耗量逐渐增加,常规油气资源已无法完全满足全社会对能源的需求^[1-4]。目前我国致密油藏资源丰富,分布范围广泛,可采储量已达40×10⁸t,主要分布在新疆油田、长庆油田等地,具有广阔的勘探开发前景^[5-8]。与常规油藏相比,致密油藏储层分布大量纳米级孔隙,且孔隙结构复杂、毛细管阻力大、原油流动困难^[9-11]。致密油藏若采用衰竭式开采,压力衰竭速度过快导致油藏开发周

期短、采收率低、剩余油含量高,在弹性开采后应采取合理的增产措施^[12-15]。同时致密油藏储层普遍水敏性较强,注水开采难度大且易对地层造成不可逆的伤害,因此注气开发逐渐受到关注^[16-20]。

目前,用于致密油藏提高采收率的气体有CO₂、N₂、天然气、烟道气、空气等。其中,CO₂是目前研究最多、效果最为理想的气体,在油藏条件下更容易达到混相条件。近年中外注气提高采收率研究如表1所示。

表1 油藏注气驱油效率汇总

Table1 Summary of oil displacement efficiency under gas injection in reservoirs

研究人员	注入气体	压力/MPa	温度/°C	采收率/%
管奕婷等 ^[21]	烃气	15.5	45	47.95
许清华 ^[22]	烃气	49.1 ~ 53.08	110 ~ 128	68.08 ~ 86.48
李德祥等 ^[23]	空气	23.8	110	55.4 ~ 61.3
PU等 ^[24]	CO ₂	4 ~ 26	75	21.2 ~ 40.9
刘鹏刚 ^[25]	空气	40	102	18
HUANG等 ^[26]	CO ₂	15	80.15	大孔隙:40 ~ 80 小孔隙:50 ~ 80
ZHOU等 ^[27]	CO ₂	12.9	44	38.96
LI等 ^[28]	CO ₂	4 ~ 14	80	39.48 ~ 91.49

大量研究结果表明,致密油藏中注CO₂及N₂一定程度均能提高采收率,其中以CO₂效果最好。但是在致密油藏储层中,天然裂缝与人工裂缝发育交错,在注气过程中常出现窜流等问题,很大程度上限制气体波及范围及驱油效率。因此,开始探索复合气体、化学助剂辅助CO₂提高采收率机理^[29-32]。GAJBHIYE通过实验手段明确CO₂/N₂混合气体对油气界面张力的变化特征,结果表明,CO₂摩尔分数的增加会降低油气两相界面张力,N₂摩尔分数的增加会增大油气两相界面张力,由此可知注入气体成分对注气提高采收率效果至关重要,在矿场实施阶段需重点考虑^[33]。

发挥注入流体间的协同(混相压力、原油膨胀)驱油优势逐渐受到重视,然而由于多流体与原油、岩石间相互作用机理复杂,微观协同提高采收率机理仍不明确^[34-36]。随着对不同注入介质-原油混相能力研究的不断深入,发现C₂H₆能够有效降低原油最小混相压力,且降低幅度高于纯CO₂^[37]。同时油田开发过程中,大量烃类气体被开采,能够保证C₂H₆具有稳定气源。因此,笔者利用高温高压PVT、黏度实验装置,研究了CO₂及复合气体(CO₂-

C₂H₆,文中的摩尔分数均为60%)-原油的饱和压力及黏度变化特征,并通过岩心吞吐实验揭示不同气体类型、吞吐压力及吞吐轮次下不同孔隙结构原油动用规律,为致密油藏注复合气体(CO₂-C₂H₆)提高采收率提供理论指导。

1 实验器材及流程

1.1 实验器材

实验用原油为地层原油和油田伴生气复配的模拟油,所用模拟油的流体特征与鄂尔多斯盆地的致密油相似。实验用岩心取自鄂尔多斯盆地现场致密砂岩岩心,岩心基础数据如表2所示。在开展物理模拟实验前,利用甲苯对岩心进行清洗,在150 °C的烘箱中对岩心进行烘干。实验仪器包括:MacroMR12-110H- I型核磁共振仪器、恒温箱、Vindum VP-3K-C型驱替泵、手摇泵、增压泵、岩心夹持器等。

1.2 实验流程

1.2.1 岩心基础物性实验

选择实际地层岩心开展基础物性实验,首选通过气测渗透率、孔隙度测量仪确定致密砂岩岩心孔

表2 岩心基础数据
Table2 Basic core data

岩心编号	长度/cm	直径/cm	干重/g
1#	5.22	2.56	54.12
2#	5.26	2.56	52.02
3#	5.35	2.56	59.21
4#	5.22	2.56	55.02
5#	6.12	2.56	53.19
6#	5.42	2.56	54.36
7#	5.24	2.56	56.68

渗数据,其次通过铸体薄片及扫描电镜明确岩心孔隙结构及矿物特征。

1.2.2 高温高压PVT实验

按照地层原油气油比在高温高压PVT反应釜中配制原始活油样品,将高温高压PVT反应釜温度升至地层温度,打开反应釜内搅拌装置并稳定6 h。利用注入泵将高温高压PVT反应釜压力升至指定压力,并稳定6 h。以恒定速度退泵,降低高温高压PVT反应釜压力,记录退泵体积与压力(稳定2 h),高温高压PVT实验装置如图1所示。

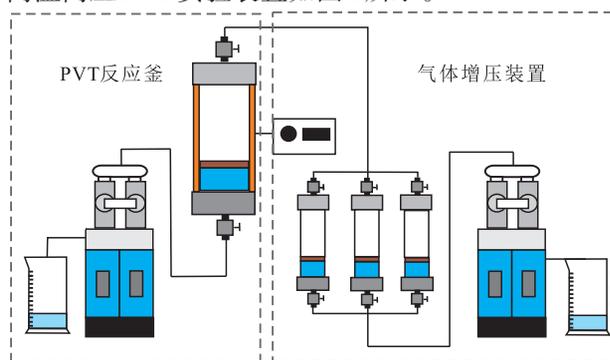


图1 高温高压PVT实验装置
Fig.1 High-temperature and high-pressure PVT experimental setup

1.2.3 高温高压黏度实验

按照地层原油气油比在高温高压PVT反应釜中配制原始活油样品,将活油样品导入螺旋管线中。利用水浴加热及升压装置,将螺旋管线温度及压力升至地层条件,并开启搅拌装置使油与气充分接触,最终通过高温高压黏度计算系统自动计算原油黏度。高温高压黏度实验装置如图2所示。

1.2.4 高温高压岩心吞吐实验

具体步骤包括:①将岩心抽真空饱和地层原油,并通过核磁共振测定原油孔隙分布。②按照摩尔分数比例(7:3)配制复合气体(CO₂-C₂H₆)。③将岩心置于高温高压岩心吞吐实验装置(图3)中,利用气体增压装置将纯CO₂及复合气体增至不同压力

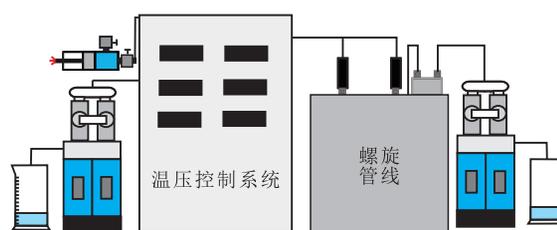


图2 高温高压黏度实验装置
Fig.2 High-temperature and high-pressure viscosity experimental setup

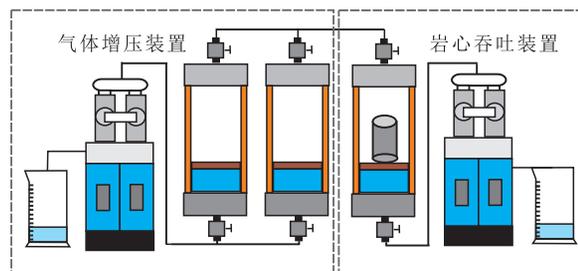


图3 高温高压岩心吞吐实验装置
Fig.3 High-temperature and high-pressure core huff and puff experimental setup

注入放有岩心的中间容器中,并稳定6 h。④稳定放压,通过称重法测定原油采收率,通过核磁共振明确剩余油动用特征。结合高压压汞与核磁共振技术^[38-40],可得到储层岩石的孔隙半径分布,而100%饱和流体的核磁共振T₂图谱可以评价孔隙半径分布。

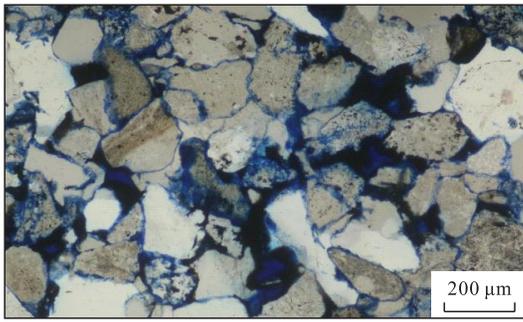
2 结果与讨论

2.1 岩心孔隙特征

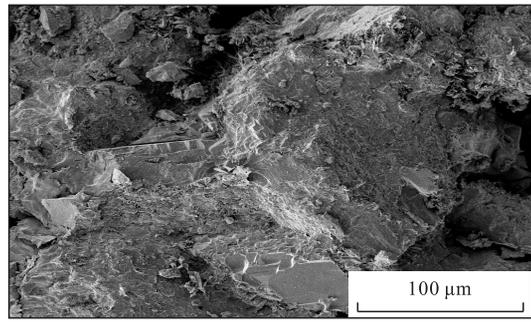
结合岩心铸体薄片及扫描电镜实验研究结果(图4),致密油藏储层岩石矿物主要由石英、斜长石、钾长石、云母、火成岩岩屑、变质岩岩屑和填隙物组成,偶见锆石、海绿石,黏土矿物颗粒微细,集中不均匀分布,粒径为0.06~0.30 mm,以细粒级为主;岩心孔隙发育中等,分布较均匀,连通性差,孔隙类型为粒间溶孔、粒间孔,少量粒内溶孔,粒间孔隙及微裂隙见自生石英、黏土矿物、伊利石、黄铁矿充填,见云母晶间微裂缝,孔隙半径为0.02~0.10 mm。

2.2 饱和压力变化特征

利用高温高压PVT实验装置,测定不同摩尔分数CO₂及复合气体(CO₂-C₂H₆)的混合原油饱和压力变化规律。由图5可知,随着CO₂摩尔分数的增加,原油饱和压力由14.03 MPa升至20.25 MPa。CO₂和60%含复合气体(CO₂-C₂H₆)的原油饱和压力分别为14.24和18.02 MPa,饱和压力上升26.54%,相同摩



a—铸体薄片实验结果



b—扫描电镜实验结果

图4 岩心孔隙特征

Fig.4 Core pore characteristics

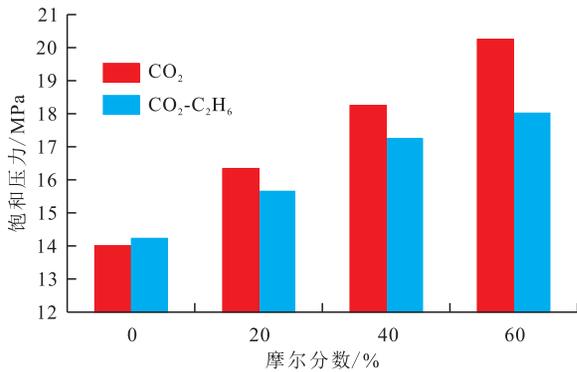


图5 原油注气时饱和压力变化

Fig.5 Saturation pressures of oil during gas injection

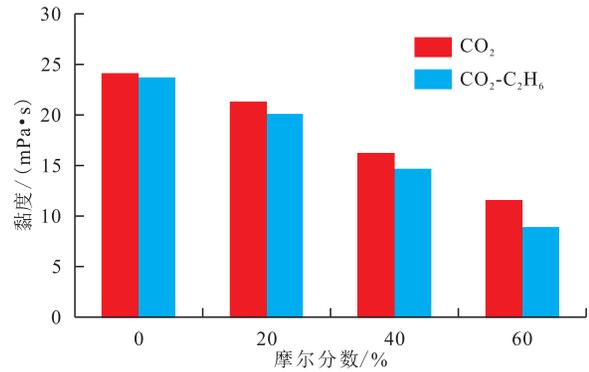


图6 原油注气时黏度变化

Fig.6 Viscosity of oil during gas injection

尔分数下,注入复合气体后的原油饱和压力均低于纯CO₂的(降低0.7~2.23 MPa)。

对比纯CO₂与复合气体(CO₂-C₂H₆)饱和压力变化规律可知,当纯CO₂注入到原油中时,CO₂溶解于原油中,CO₂分子与原油中的烃类分子相互作用,增加原油分子间吸引力,同时改变原油组分的相对含量,进而导致原油饱和压力的增加,且随着注入气体摩尔分数的上升,饱和压力逐渐增大。相同摩尔分数条件下,复合气体(CO₂-C₂H₆)的饱和压力低于纯CO₂的。由此可知,C₂H₆气体能够增加CO₂在原油中的溶解能力,增强CO₂分子在原油分子间的相互作用能力,提高油气混相能力,从而强化储层原油动用程度。

2.3 黏度变化特征

利用高温高压黏度实验装置,测定不同摩尔分数CO₂及复合气体(CO₂-C₂H₆)的混合原油黏度变化规律。由图6可知,随着CO₂摩尔分数的增加,原始油样的黏度由24.06 mPa·s降至11.55 mPa·s,黏度下降52%。CO₂和复合气体(CO₂-C₂H₆)的原油黏度分别为23.68和8.76 mPa·s,黏度下降63%。相同摩尔分数下,注入复合气体后的原油黏度均低于纯CO₂的(降低1.02~2.79 mPa·s)。

对比CO₂与复合气体(CO₂-C₂H₆)黏度变化规律

可知,当CO₂注入原油中时,CO₂溶解于原油中,能够使原油间的分子力部分转化为气-液分子间的引力,以降低原油间的内摩擦力从而起到降黏效果。随着气体摩尔分数的增加,溶解于原油中的CO₂逐渐增多,进而导致原油黏度不断降低。相同摩尔分数条件下,复合气体(CO₂-C₂H₆)的黏度均低于纯CO₂的。由此可知,C₂H₆气体增强了CO₂对原油的降黏能力,增加了原油的流动性,从而提高原油采收率。

2.4 岩心吞吐提高采收率变化特征

由图7可知,随着吞吐轮次的增加,采收率逐步增大。岩心赋存原油主要在第1,2轮次被大面积动用,第3,4轮次原油动用程度较低。随着吞吐压力的上升,CO₂-原油混相程度增强,原油黏度降低,使岩心原油采收率逐渐升高。由原油最小混相压力研究结果可知,CO₂-原油最小混相压力约为16 MPa。由CO₂吞吐实验研究结果可知,当吞吐压力高于16 MPa时,吞吐采出程度明显增加。

由图8可知,岩心赋存原油主要在第1,2轮次被大面积动用,第3,4轮次原油动用程度较低。由原油最小混相压力研究结果可知,复合气体(CO₂-C₂H₆)-原油最小混相压力约为14 MPa,当吞吐压力高于14 MPa时,采收率明显增加。

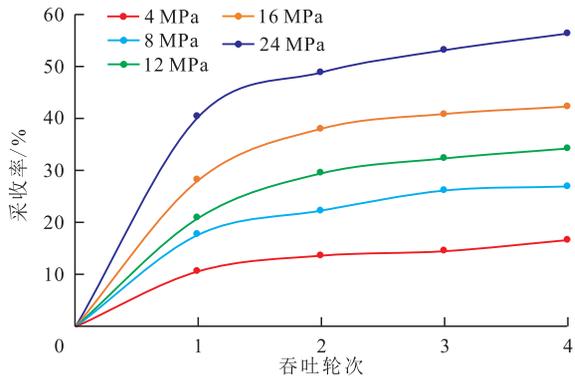


图7 岩心CO₂吞吐实验结果

Fig.7 Results of core experiments under CO₂ huff and puff

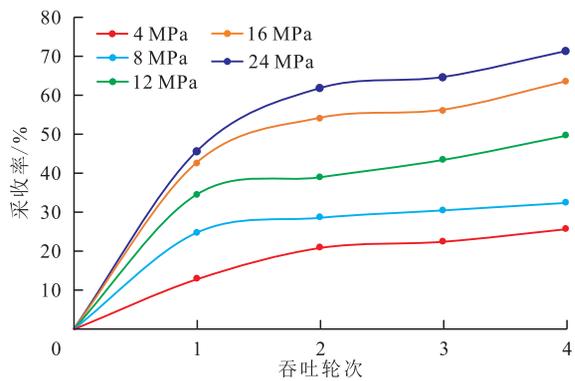


图8 岩心CO₂-C₂H₆吞吐实验结果

Fig.8 Results of core experiments under CO₂-C₂H₆ huff and puff

CO₂及复合气体(CO₂-C₂H₆)在不同吞吐压力(分别为4,8,12,16和24 MPa)下经4轮吞吐后采收率如图9所示。对比岩心CO₂与复合气体吞吐实验结果可知,由于C₂H₆能够增强CO₂在原油中的溶解度,减小原油分子的内摩擦阻力,从而增强CO₂对原油的降黏能力,进而提高岩心原油动用程度,使相同吞吐条件(压力、轮次)下复合气体提高原油采收率程度高于CO₂(复合气体为71.43%;CO₂为56.38%),且压力在最小混相压力附近时采收率提高程度最大。

岩心吞吐核磁共振实验研究结果如图10和图

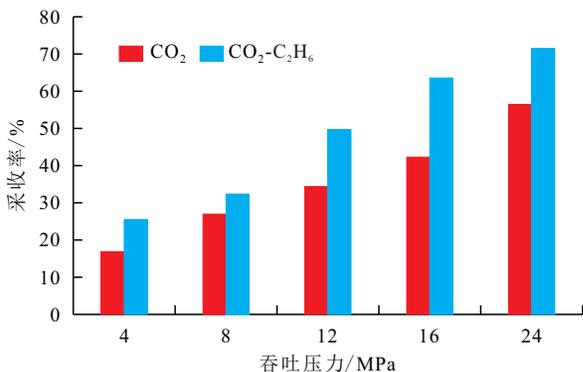


图9 不同吞吐压力下吞吐提高采收率变化特征

Fig.9 Oil recoveries under different gas huff and puff

11所示。由I类储层典型岩心在不同吞吐压力下吞吐至剩余油状态时的核磁共振T₂图谱可知,I类储层孔喉集中分布在0.0001~0.001,0.01~1 μm,随着吞吐压力的逐渐升高,不同孔喉原油均得到有效动用。由图10可知,吞吐压力小于8 MPa时,CO₂主要动用0.01~1 μm孔喉中赋存的原油,0.0001~0.001 μm内赋存的原油动用程度较小。随着吞吐压力的逐渐增加,0.0001~0.001 μm内赋存的原油逐渐动用,且当吞吐压力在CO₂-原油最小混相压力附近时该孔喉原油动用程度较高。相较于CO₂,复合气体(CO₂-C₂H₆)对原油的降黏程度更高,且加入C₂H₆能够更大程度降低原油最小混相压力,因此复合气体对0.0001~0.001,0.01~1 μm孔喉中的原油动用程度均强于CO₂的(图11)。

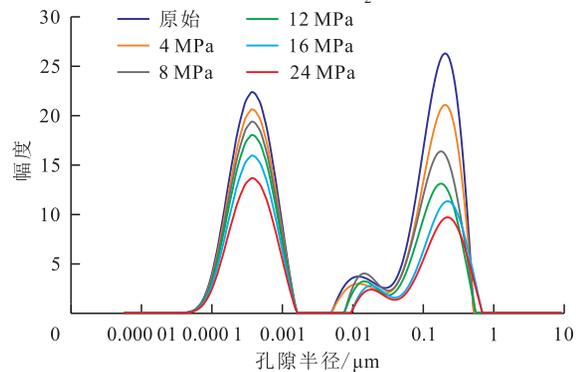


图10 CO₂吞吐核磁共振T₂图谱

Fig.10 NMR T₂ spectrum under CO₂ huff and puff

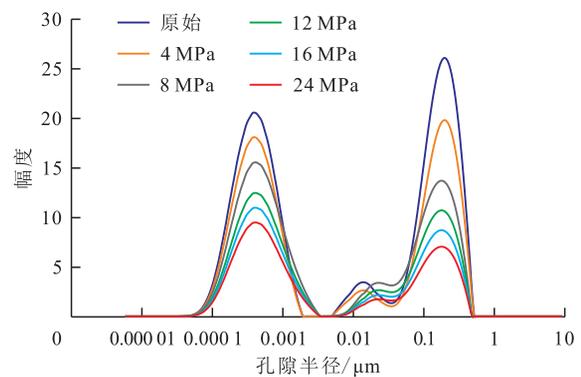


图11 CO₂-C₂H₆吞吐核磁共振T₂图谱

Fig.11 NMR T₂ spectrum under CO₂-C₂H₆ huff and puff

不同孔喉中CO₂及复合气体(CO₂-C₂H₆)吞吐提高原油采收率效果(图12)表明,0.01~1 μm孔喉原油采收率提高程度均高于0.0001~0.001 μm(0.01~1 μm:8%~46%;0.0001~0.001 μm:20%~68%),且岩心已知孔喉处复合气体吞吐提高采收率程度均高于CO₂的(相较于CO₂约提高5%~10%)。

对比CO₂及复合气体在不同孔喉处的原油采收率可知,致密砂岩储层不同孔喉的原油均可通过CO₂或复合气体吞吐技术实现有效动用,且随着吞

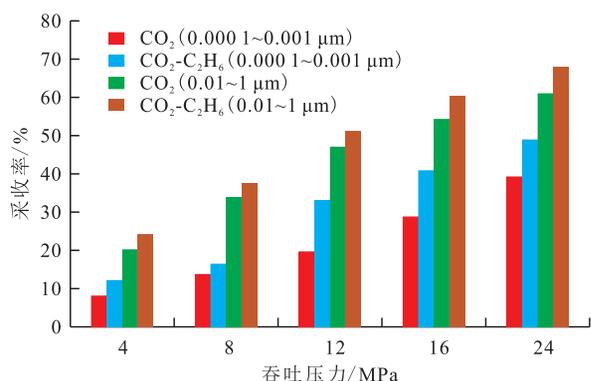


图 12 不同孔喉吞吐提高采收率变化特征

Fig.12 Oil recoveries of different pores under huff and puff

吐压力的不断上升,气体大量溶解于原油中,降低原油分子间的内摩擦力,从而降低原油黏度,提高原油流动能力。同时CO₂及复合气体均能够与原油实现混相,大幅度降低油气界面张力,从而提高原油动用程度。相比于CO₂吞吐,C₂H₆气体能够提高复合气体与原油间的溶解、降黏及混相程度,将CO₂吞吐无法动用的剩余油携带出储层,且当吞吐压力接近最小混相压力时,原油采收率变化程度最高。

3 结论

随着注入气体摩尔分数的上升,饱和压力逐渐增大。相同摩尔分数条件下,复合气体(CO₂-C₂H₆)的饱和压力低于纯CO₂的。C₂H₆气体能够增加CO₂在原油中的溶解能力,从而强化储层原油动用程度。随着气体摩尔分数的增加,溶解于原油中的CO₂逐渐增多,进而导致原油黏度不断降低。相同摩尔分数条件下,注入复合气体(CO₂-C₂H₆)的原油黏度均低于纯CO₂的。C₂H₆气体增强了CO₂对原油的降黏能力,增加了原油的流动性,从而提高原油采收率。

岩心赋存原油主要在第1,2轮次被大面积动用,且吞吐压力在油气最小混相压力附近,原油采收率明显增加。C₂H₆能够增强CO₂在原油中的溶解度,减小原油分子的内摩擦阻力,从而增强CO₂对原油的降黏能力,进而提高岩心原油动用程度。在不同吞吐压力下,复合气体(CO₂-C₂H₆)的采收率提高效果均高于纯CO₂的(复合气体的为71.43%;纯CO₂的为56.38%),且吞吐压力在最小混相压力附近采收率提高程度高于其他吞吐压力。致密油藏储层孔喉集中分布在0.0001~0.001和0.01~1 μm中,随着吞吐压力的逐渐升高,不同孔喉原油均得到有效动用。相较于纯CO₂,复合气体(CO₂-C₂H₆)吞吐

对0.0001~0.001和0.01~1 μm孔喉中的原油动用程度更强,能够将纯CO₂吞吐无法动用的剩余油携带出储层,是未来致密油藏高效开发的一种有效技术。

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